



**Jet Propulsion Laboratory**  
California Institute of Technology

# Origami wrapping patterns for non-planar unfolded forms

Manan Arya

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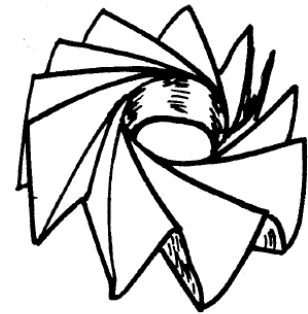
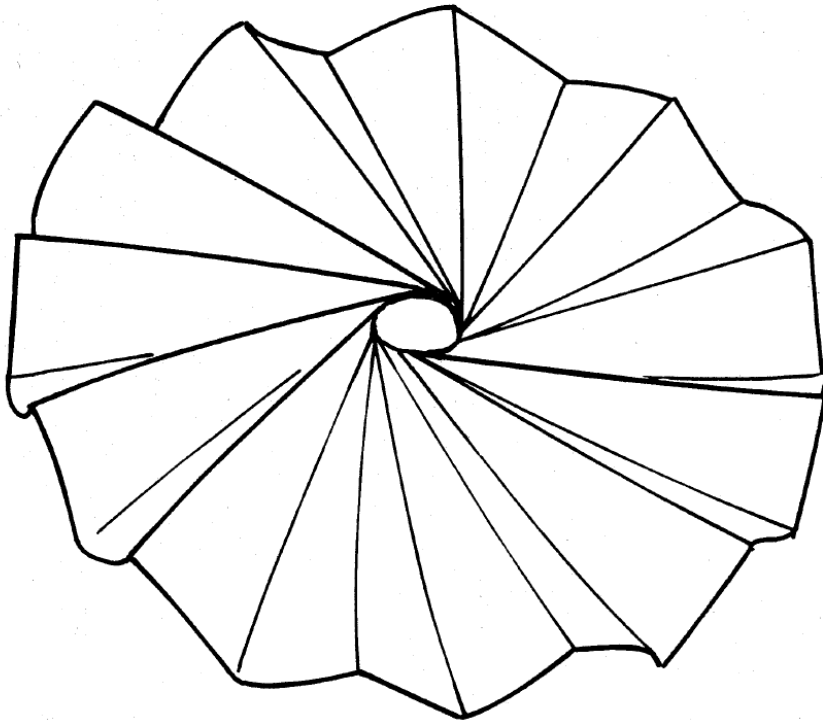
Engineering Mechanics Institute Conference 2019

19 June 2019

Pasadena, California

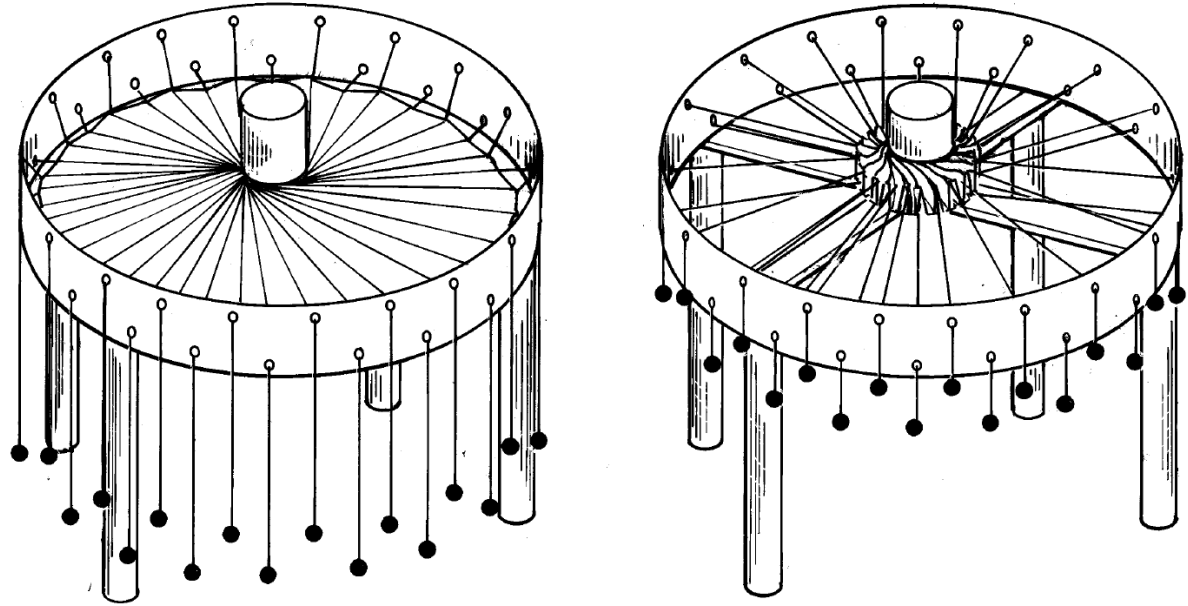
# What is an origami wrapping pattern?

- Wraps sheet-like materials around a central body
- Generally, exhibits N-fold rotational symmetry



# Origami wrapping patterns

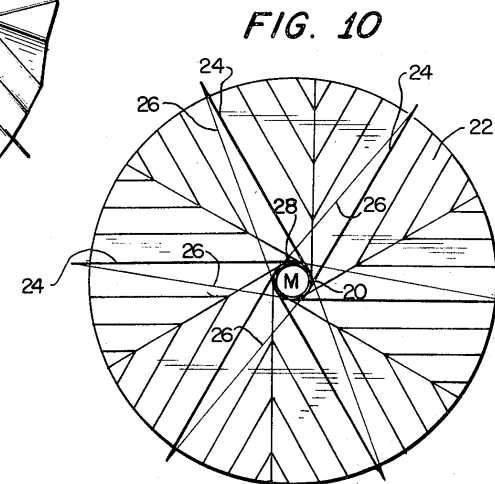
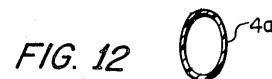
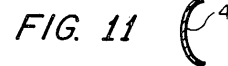
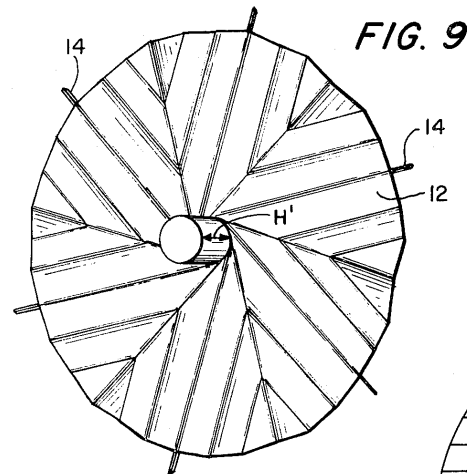
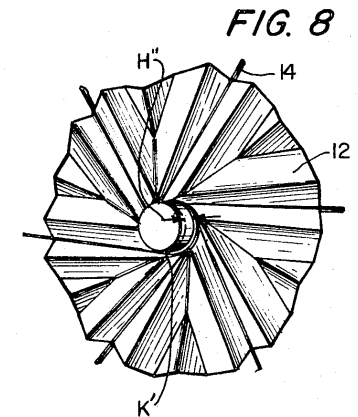
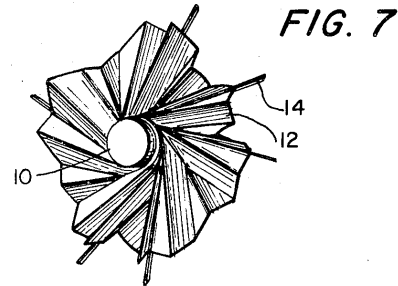
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W.E. Lanford, "Folding apparatus", U.S. Patent 3010372, 1961.

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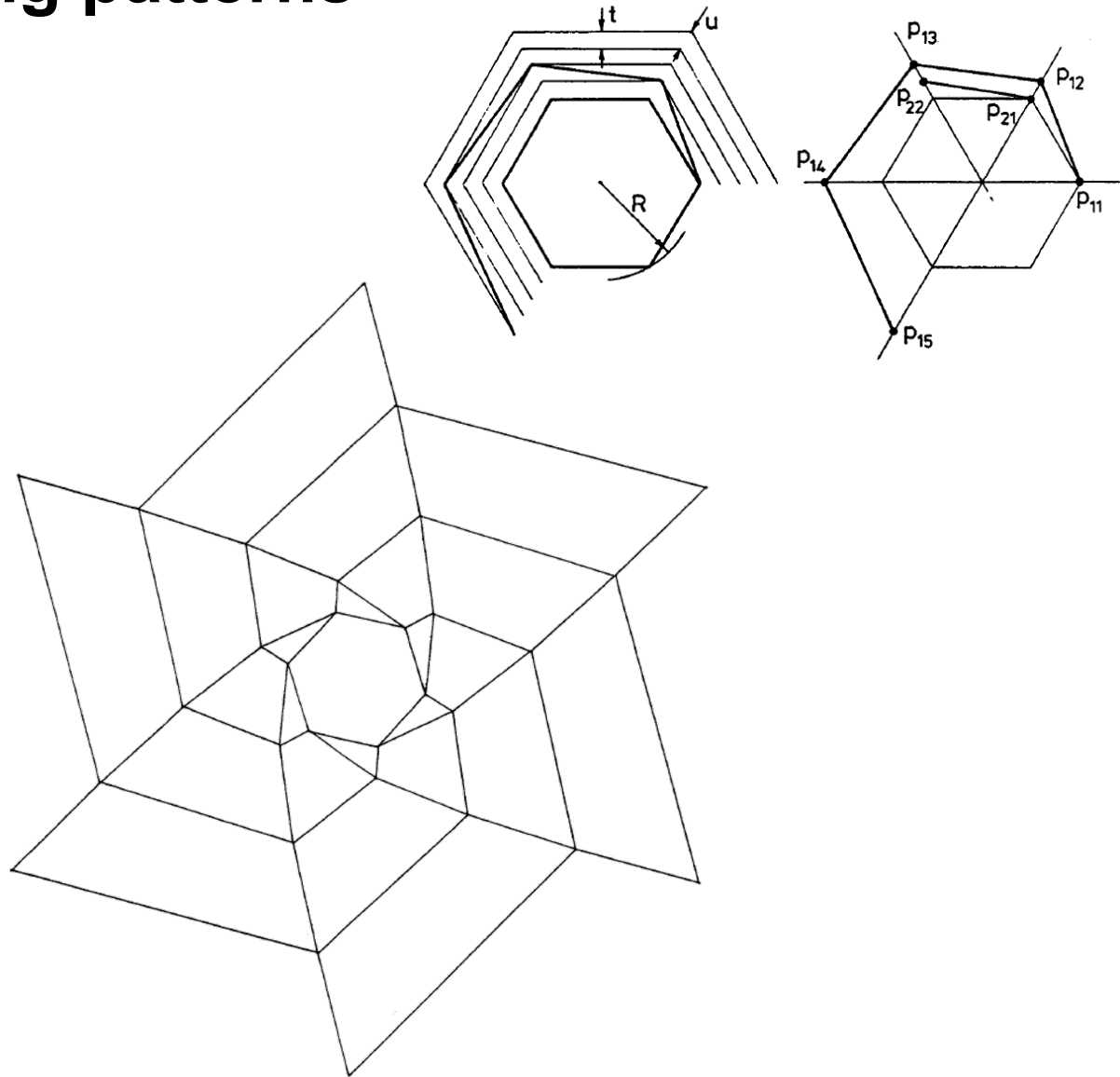
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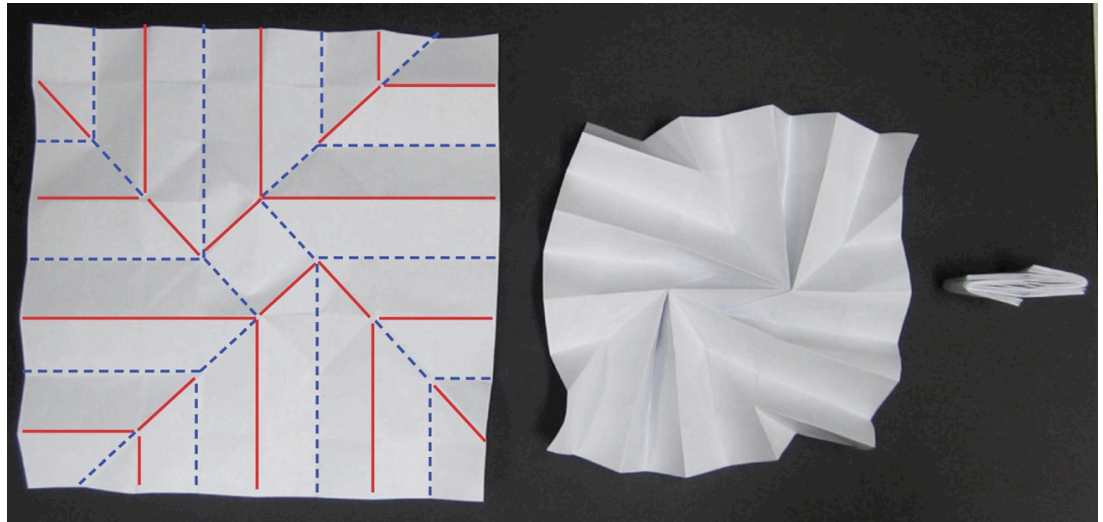
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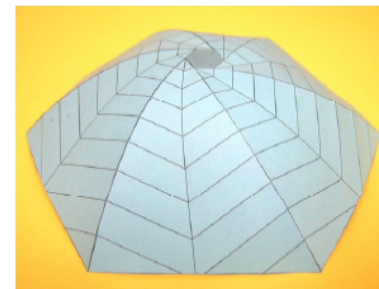
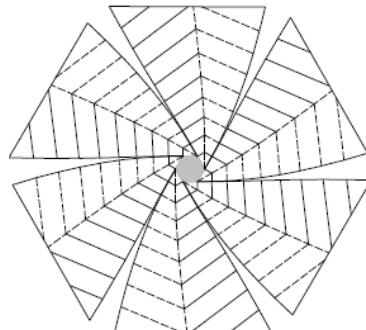
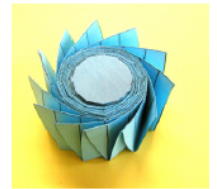
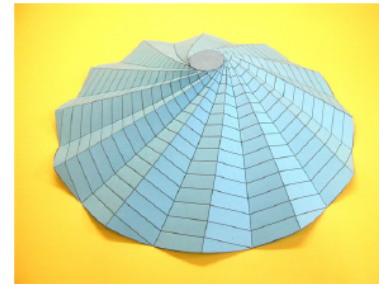
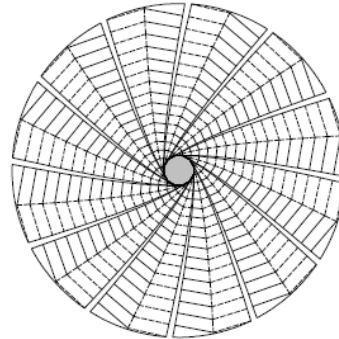
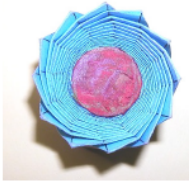
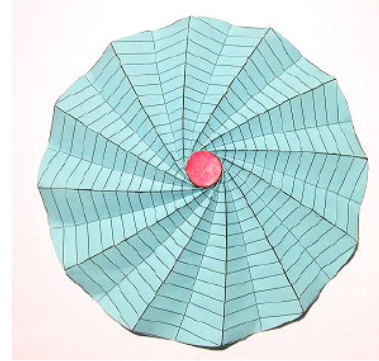
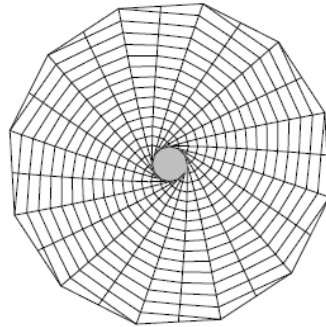
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From, S. A. Zirbel *et al.*, “Accommodating Thickness in Origami-Based Deployable Arrays,”  
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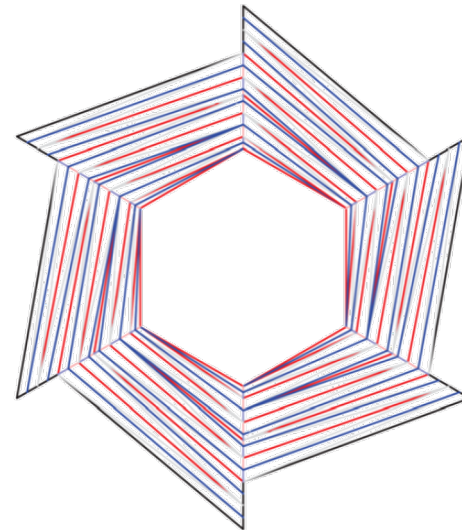
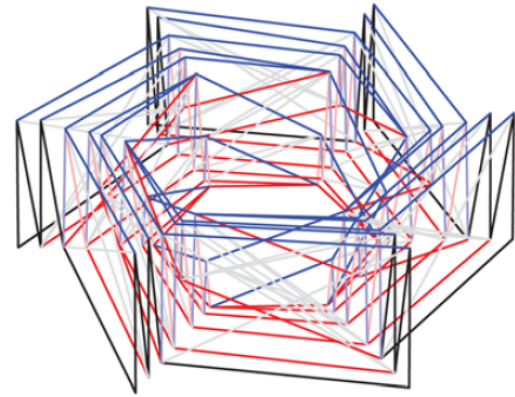
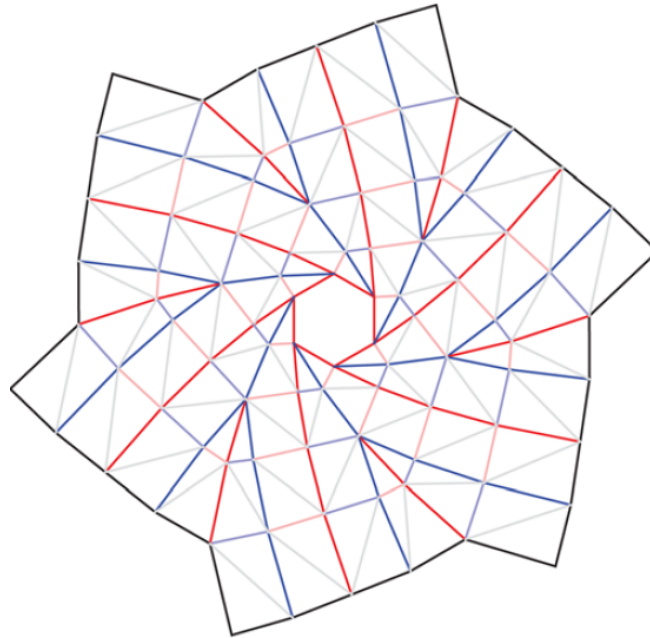
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# Motivation

- Deployable solar arrays for spacecraft
  - Enable high-power solar arrays to be folded compactly for launch



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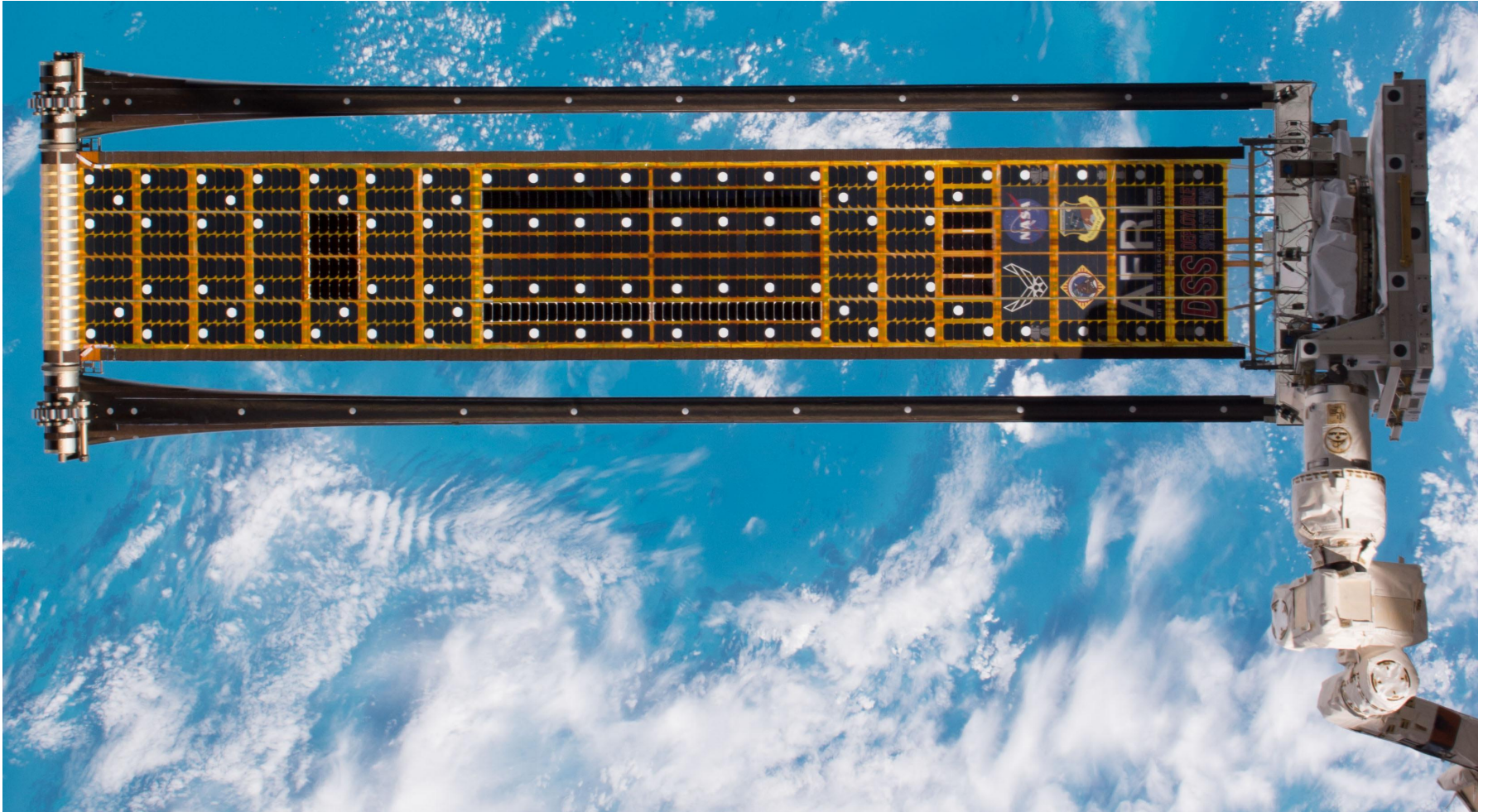
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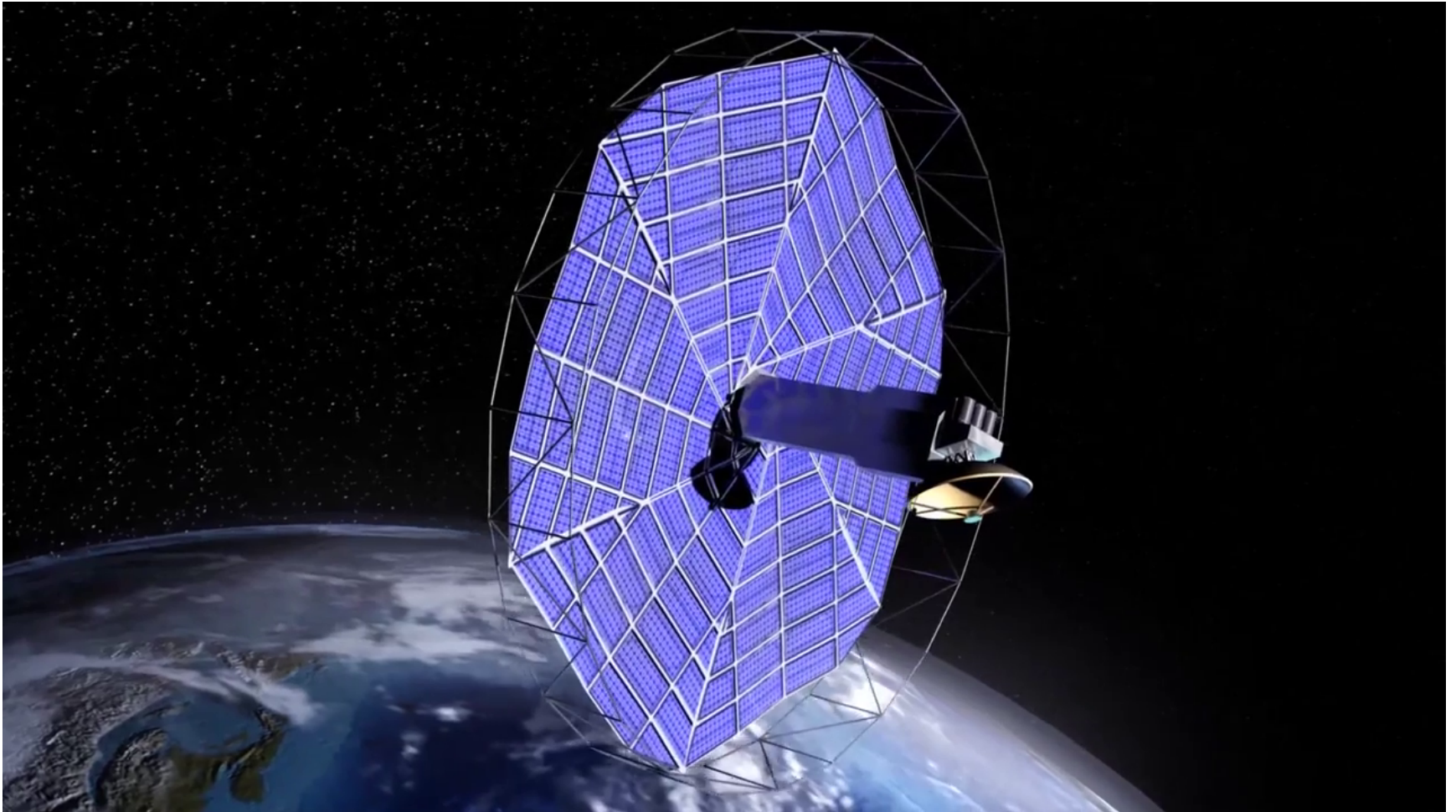
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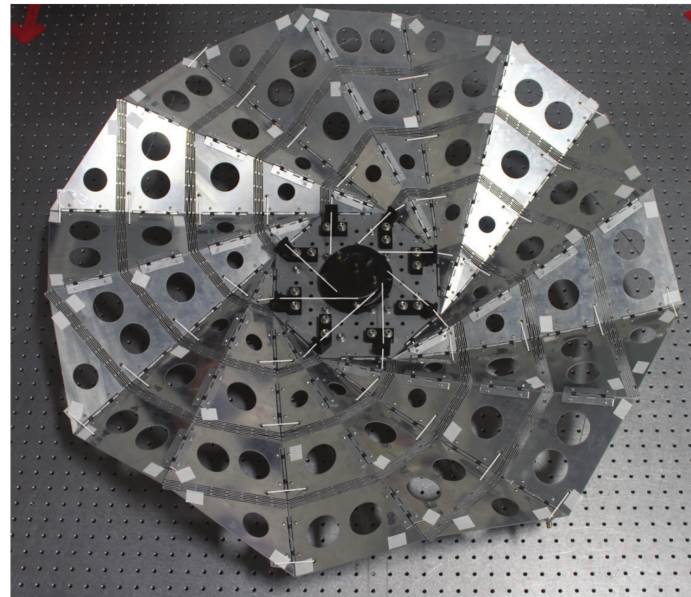
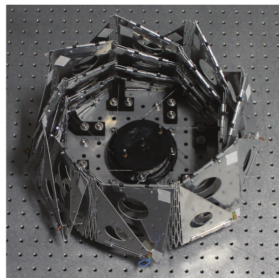
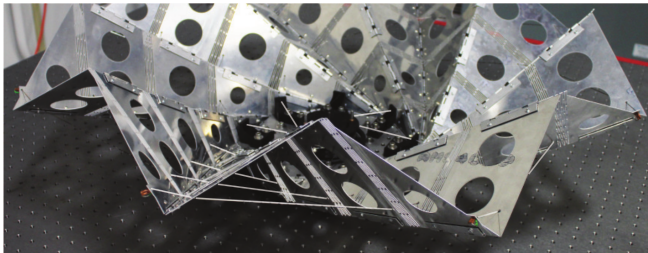


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- Deployable solar arrays for spacecraft
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- Thin, planar unfolded forms require a separate structure to provide out-of-plane stiffness
  - e.g. deployable trusses, booms, masts
- Mass, complexity, volume savings if this separate structure was not needed

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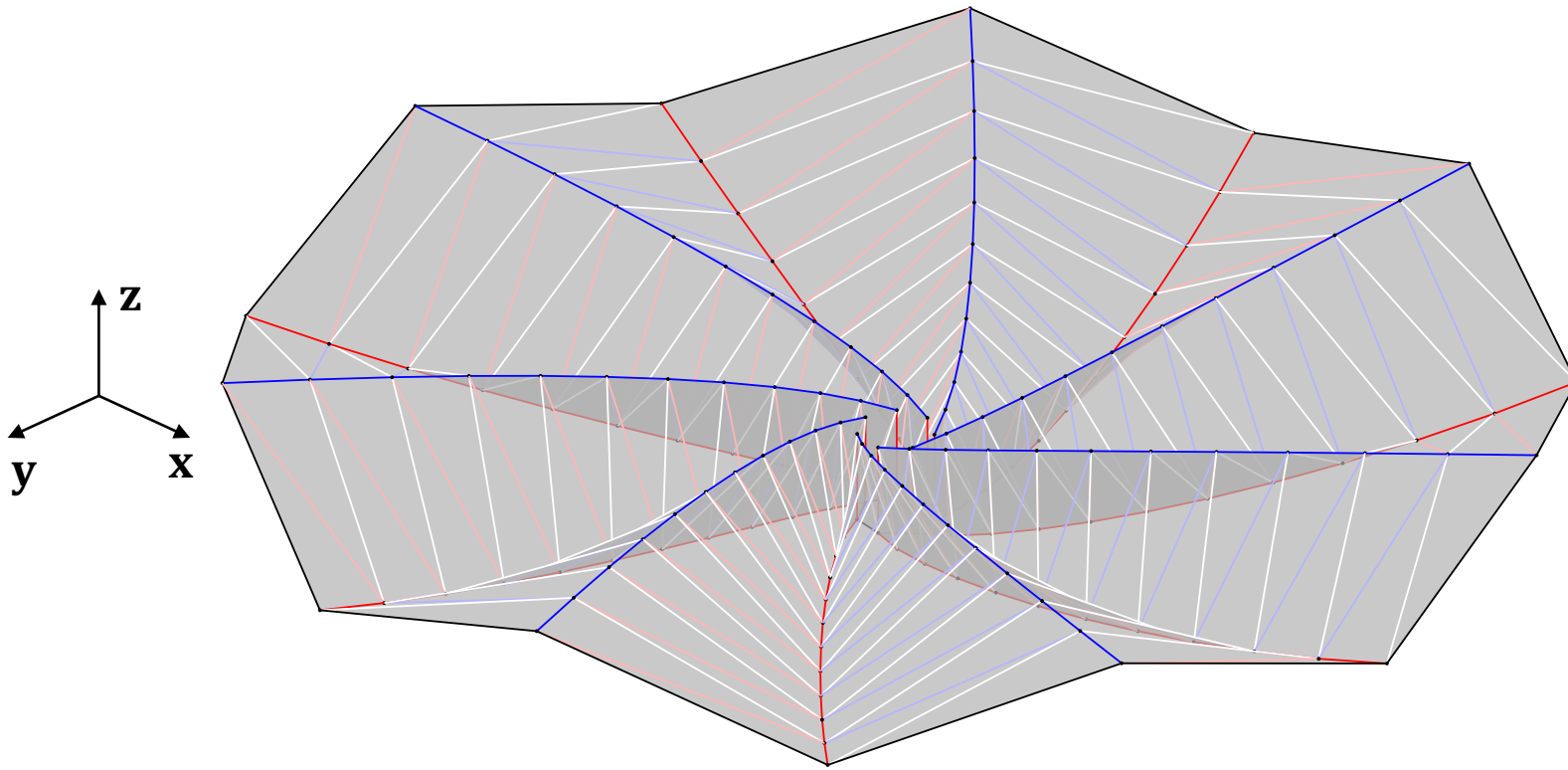
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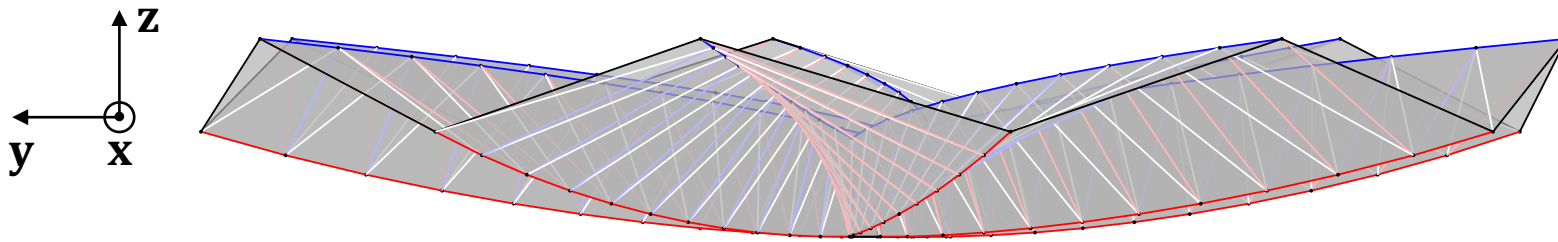
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- Mass, complexity, volume savings if this separate structure was not needed
- Partially-unfolded wrapping patterns exhibit increased bending stiffness due to out-of-plane corrugations
  - Previously achieved by tension ties to prevent full unfolding
- Can an origami pattern be designed that has a non-planar corrugated form by design?

# Concept overview

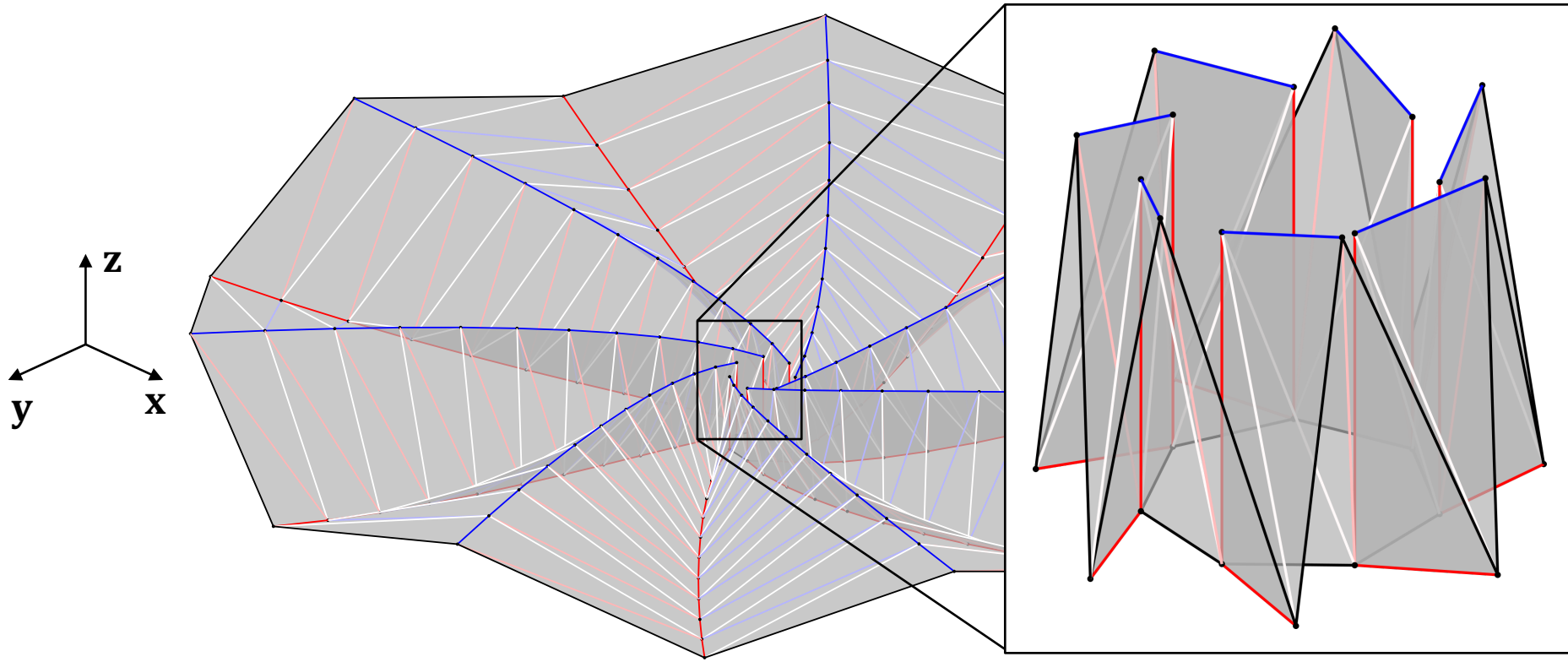


Unfolded form, isometric view

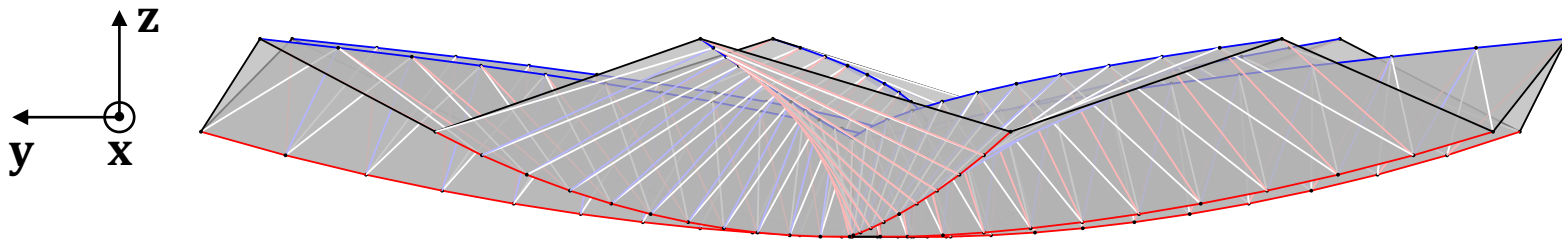


Unfolded form, side view

# Concept overview

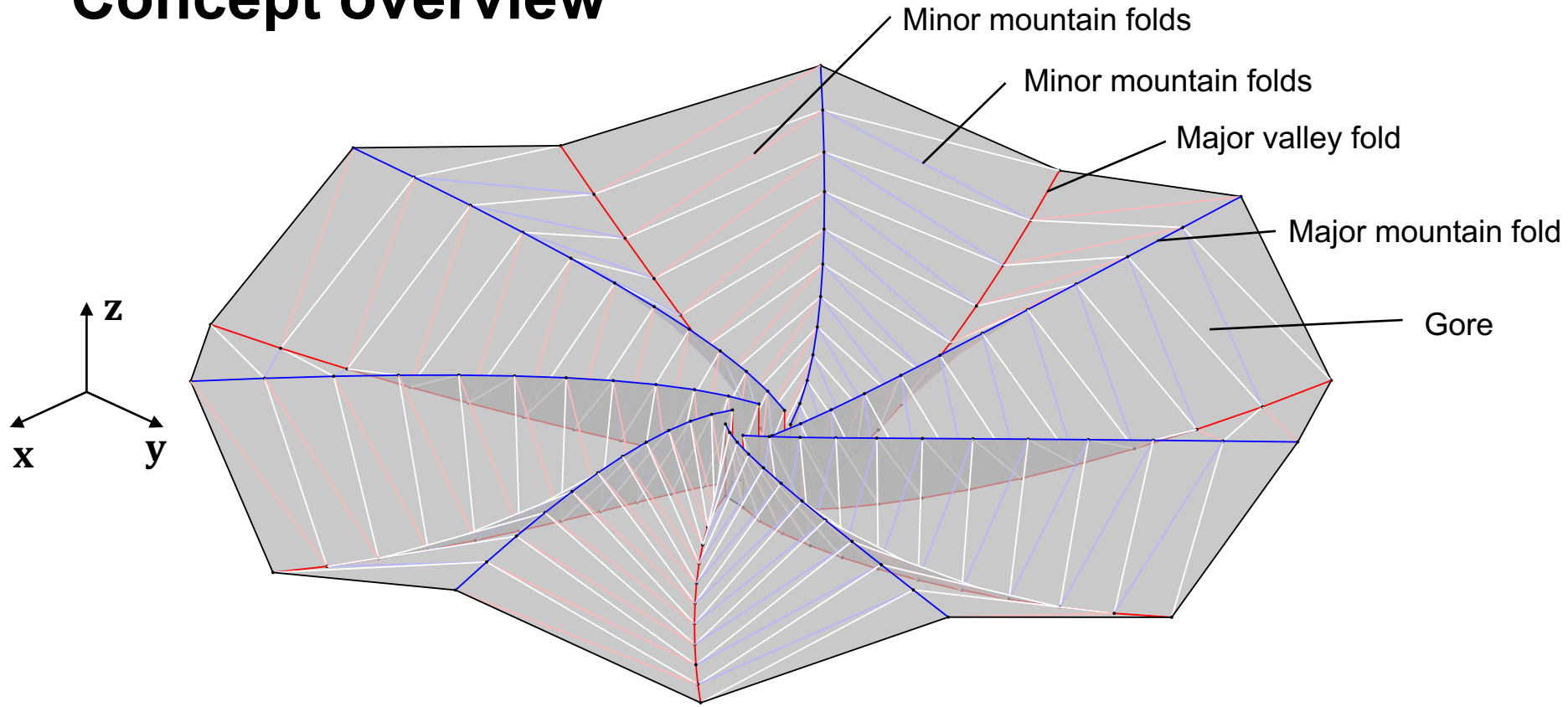


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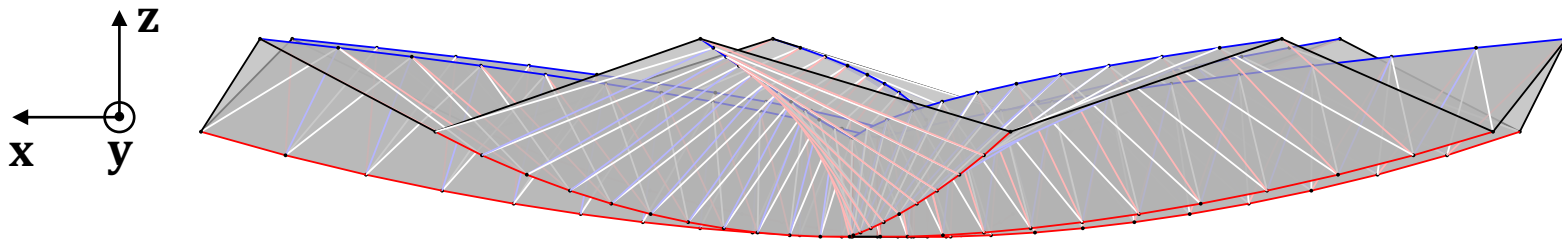


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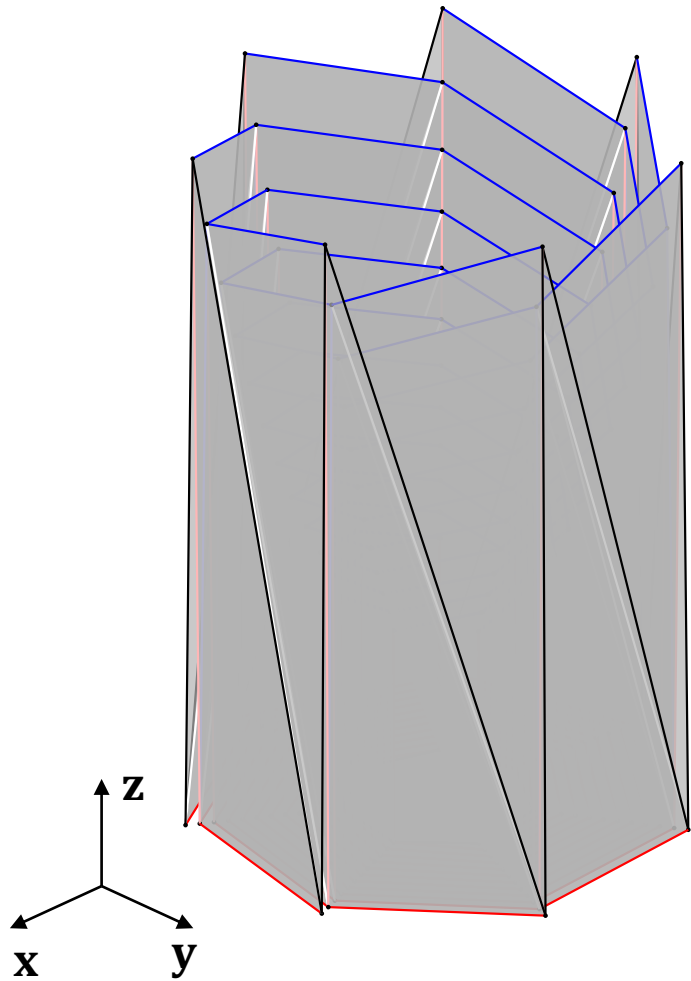
Unfolded form, isometric view



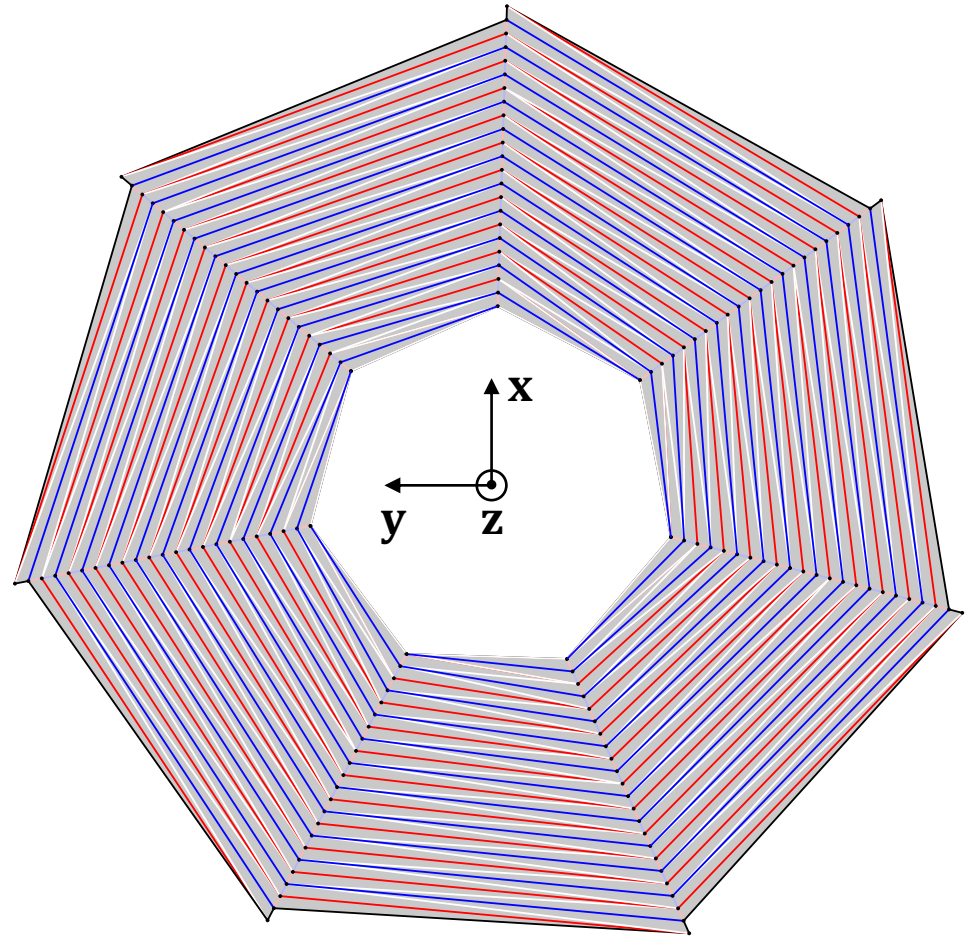
Unfolded form, side view



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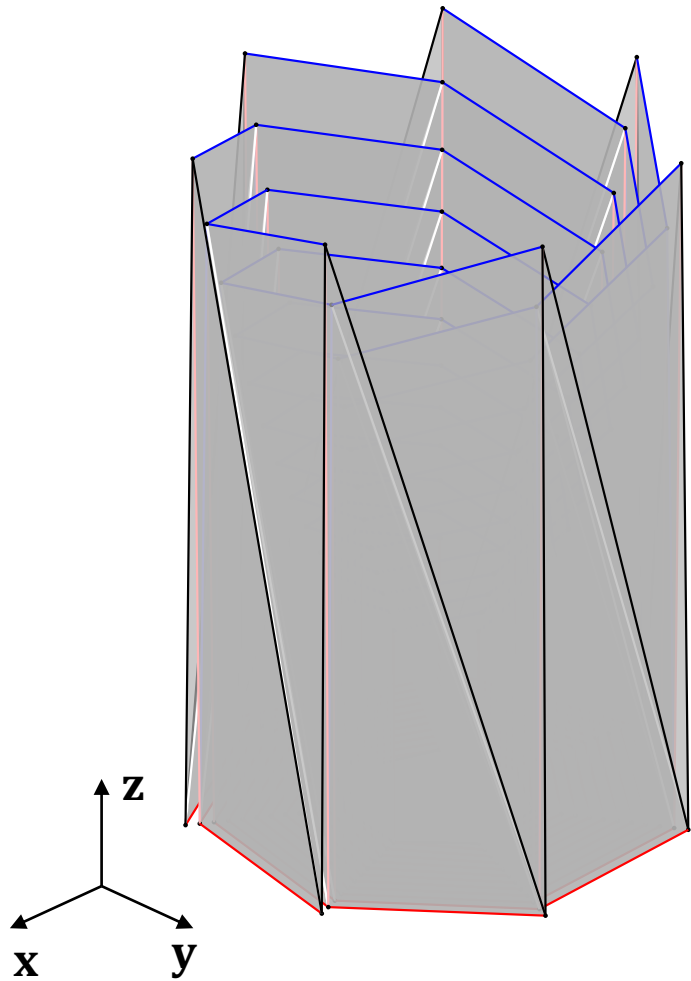


Folded form, isometric view

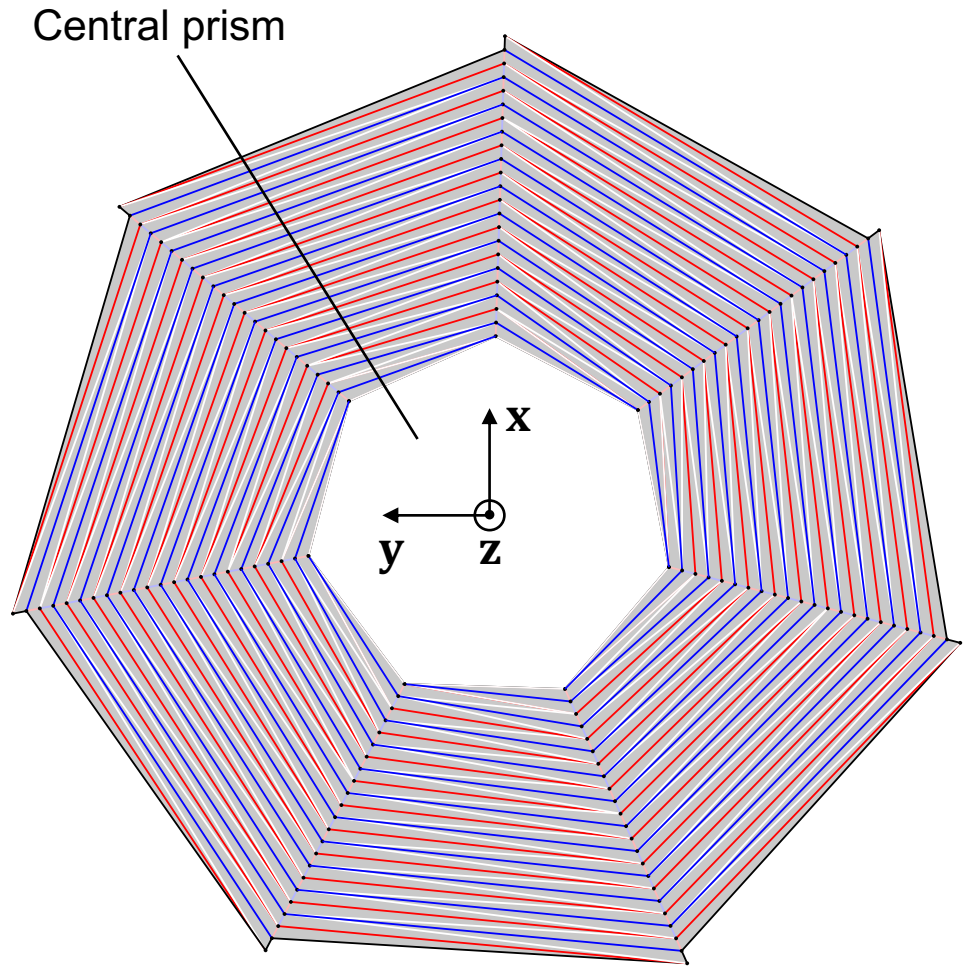


Folded form, top view

# Concept overview



Folded form, isometric view

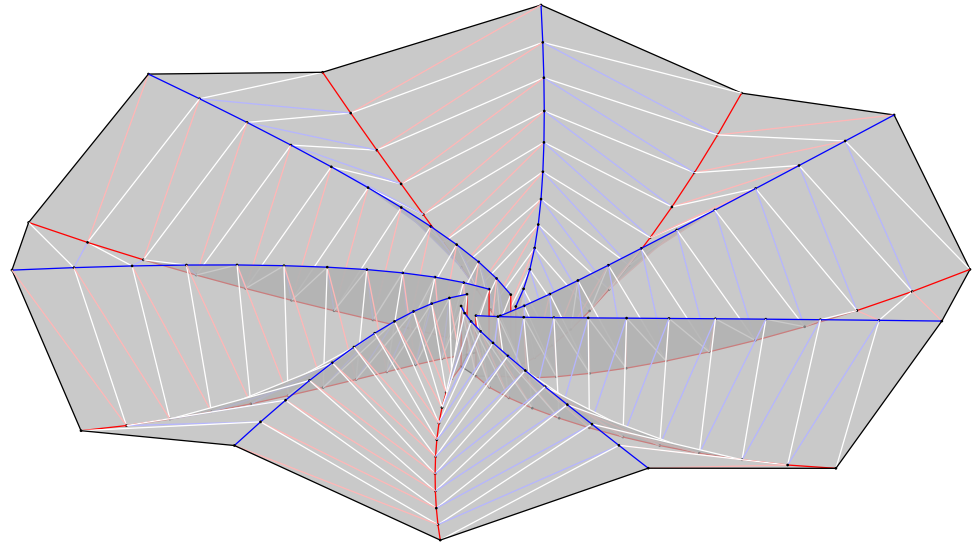
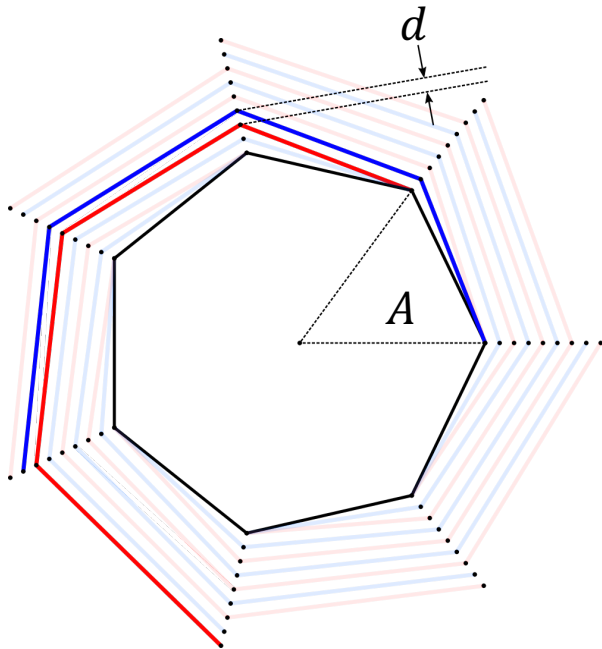


Folded form, top view

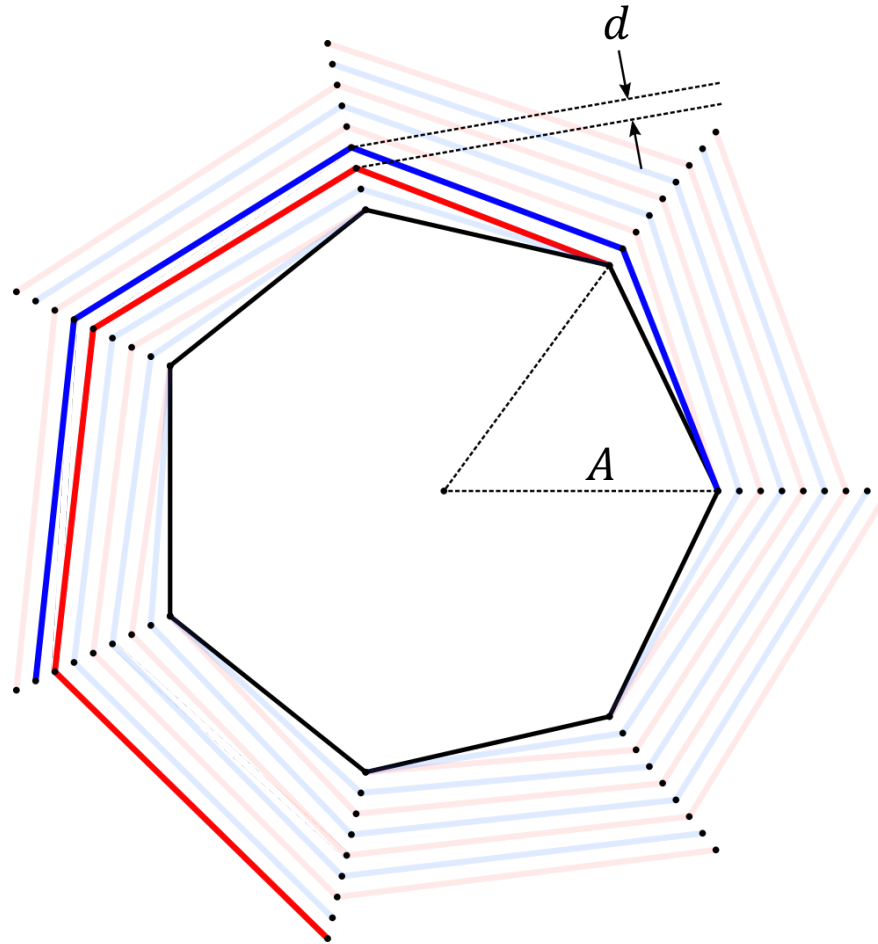


# Free parameters

$N$	Number of sides in the central prism
$n$	Number of panels in a gore
$A$	Radius of central cylinder
$d$	Radial spacing between successive folded layers
$z_0$	Height of the first mountain node
$mz_{\text{target}, i}$	Target heights of the unfolded mountain nodes, $i = 1, 2, \dots n$
$vz_{\text{target}, i}$	Target heights of the unfolded valley nodes, $i = 1, 2, \dots n$



# Folded form assumptions

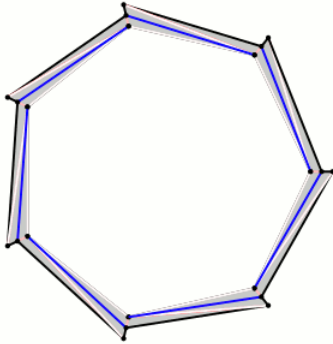


$$m_i = \mathbf{R}^i \begin{bmatrix} A + d(2i - 1) \\ 0 \\ m_i \cdot \mathbf{z} \end{bmatrix}$$

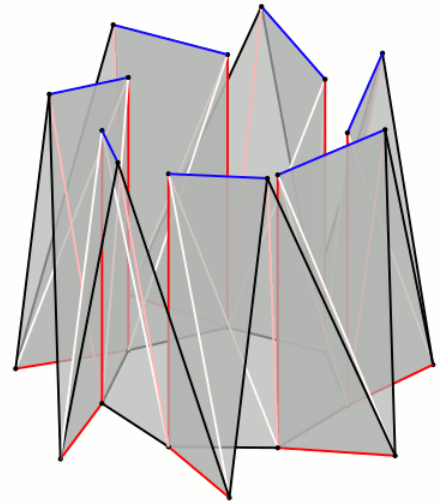
$$v_i = \mathbf{R}^i \begin{bmatrix} A + d(2i) \\ 0 \\ 0 \end{bmatrix}$$

# Algorithm design

- Generate the fold pattern from the inside out



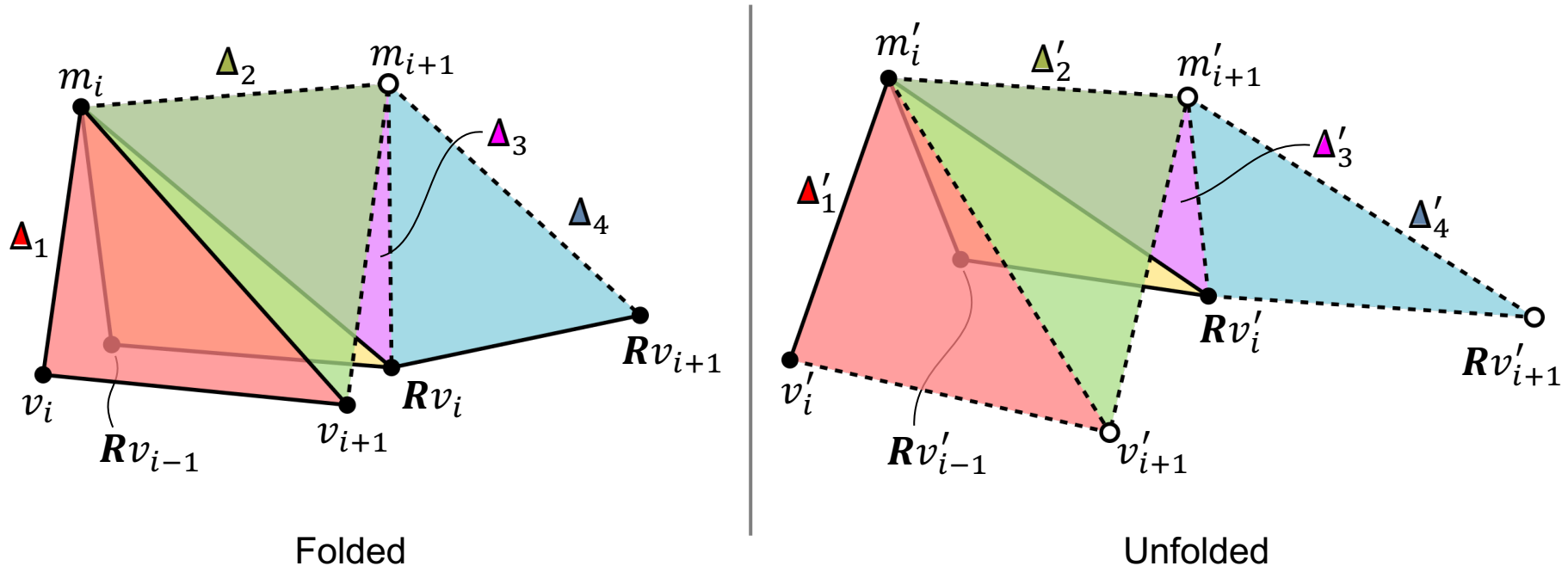
Folded



Unfolded

# Algorithm design

- Assuming known  $m_i, v_i$ , find  $m_{i+1}, v'_{i+1}, m'_{i+1}$



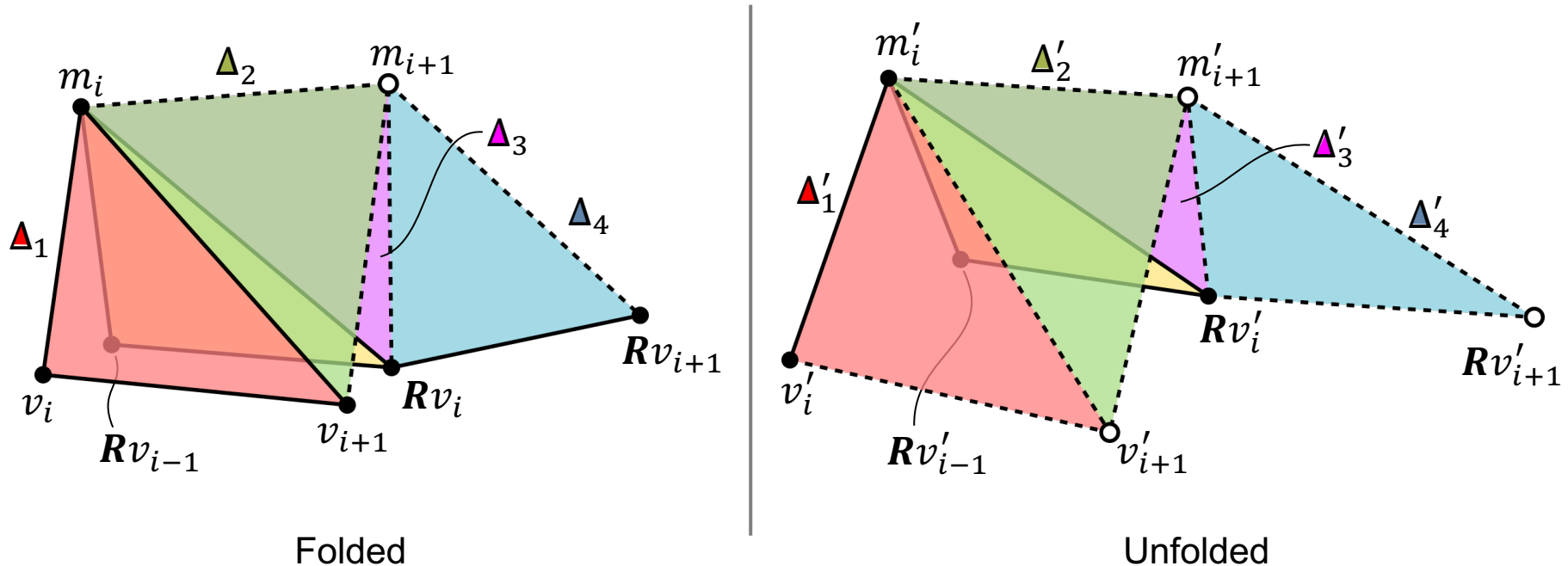
$$\text{minimize}(|m'_{i+1} \cdot \mathbf{z} - m_{\text{target}, i+1}| + |v'_{i+1} \cdot \mathbf{z} - v_{\text{target}, i+1}|)$$

over the variable  $(m_{i+1} \cdot \mathbf{z})$

such that  $\Delta_i = \Delta'_i$  for  $i = 1, 2, 3, 4$

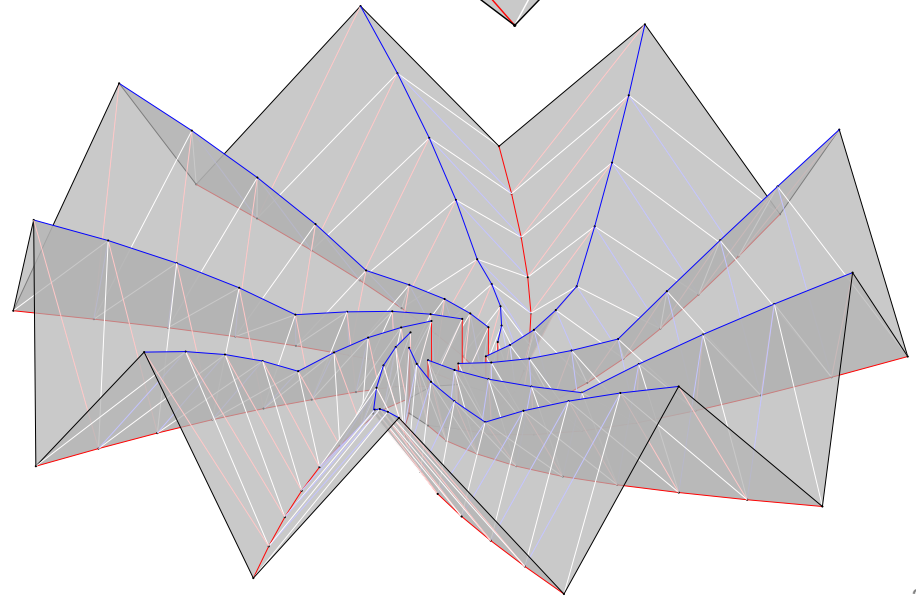
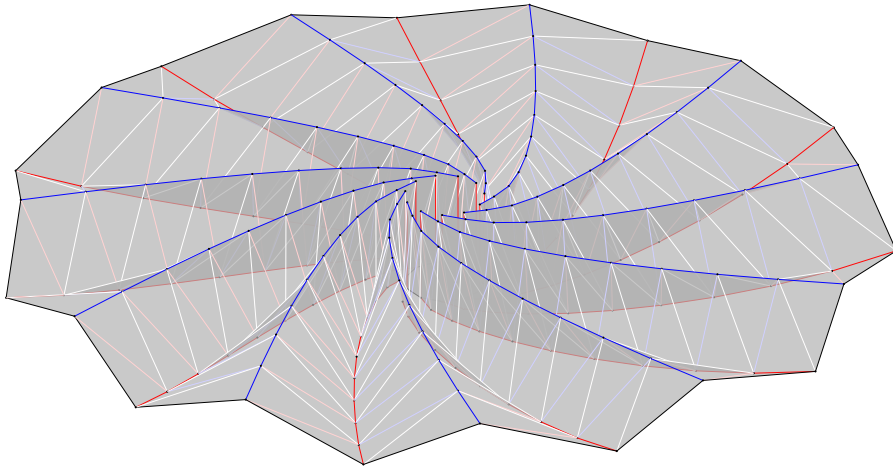
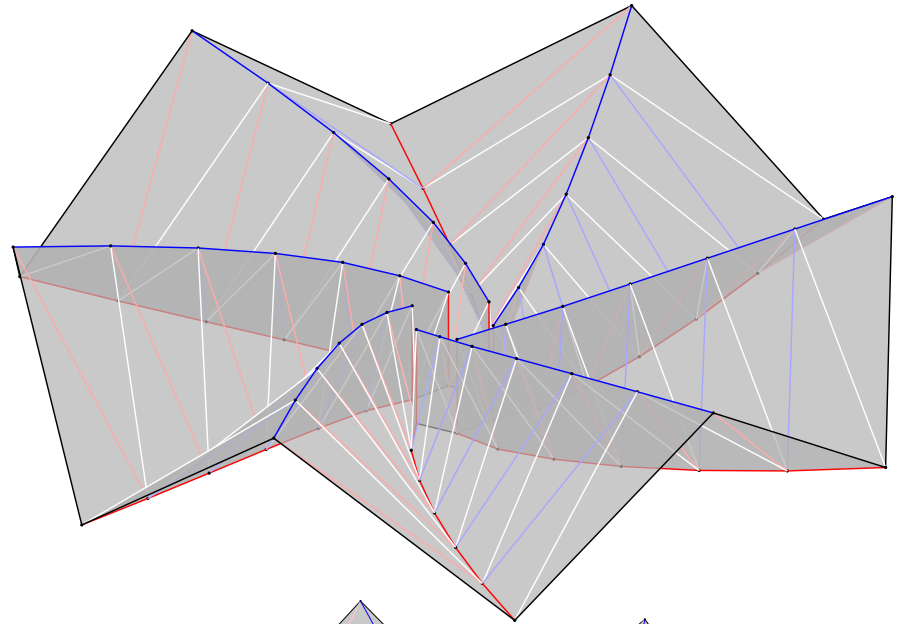
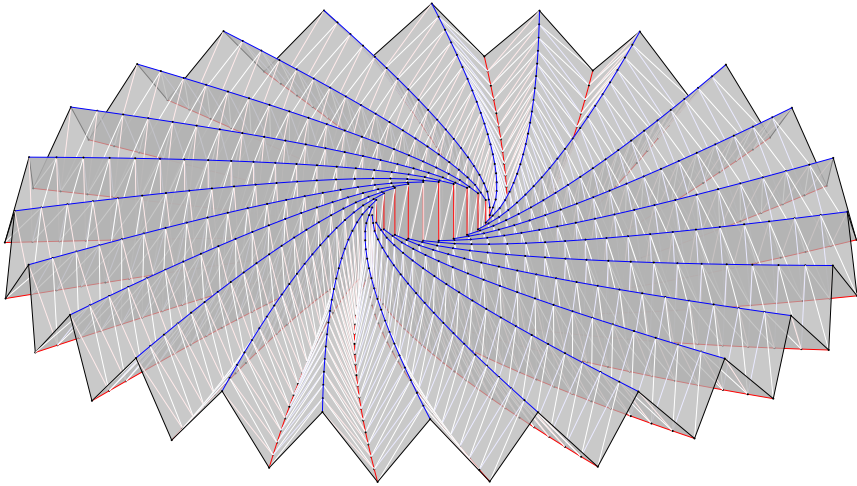
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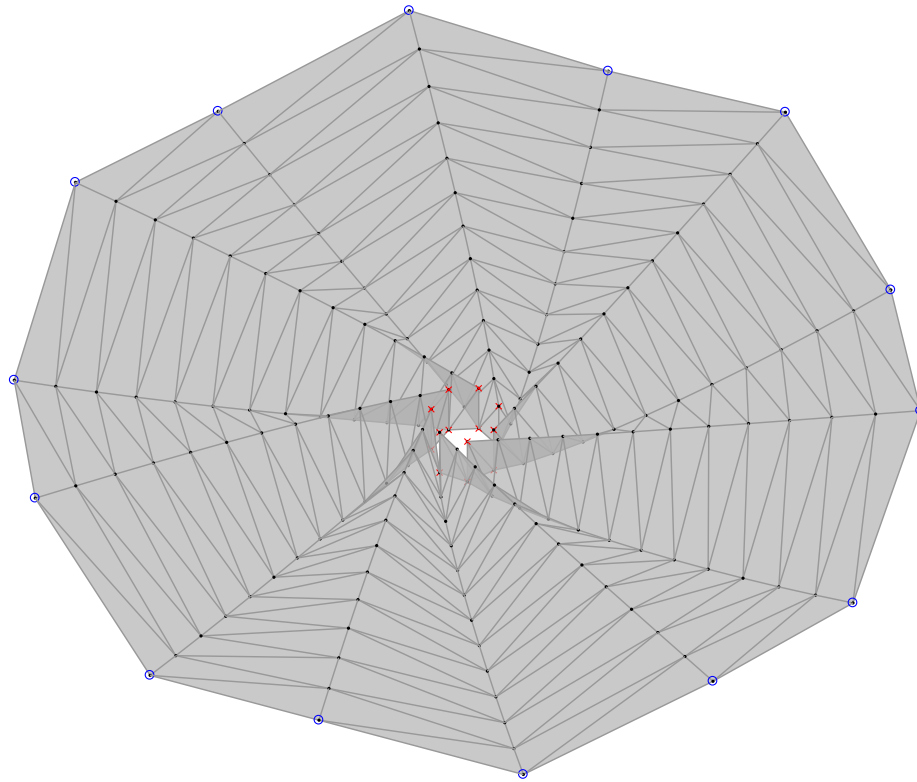
```
[m'_{i+1}, v'_{i+1}] = function generateFoldedPoints(m'_{i+1} · z)
[c] = function costFunction(m'_{i+1}, v'_{i+1}, mZ_target,i+1, vZ_target,i+1)
[(m'_{i+1} · z)*] = minimize(costFunction(generatedFoldedPoints(m'_{i+1} · z))
```

# Non-planar origami wrapping zoo



# Deployed stiffness

- Innermost valley and mountain nodes are fixed
- Equal vertical loads applied to outermost valley and mountain nodes

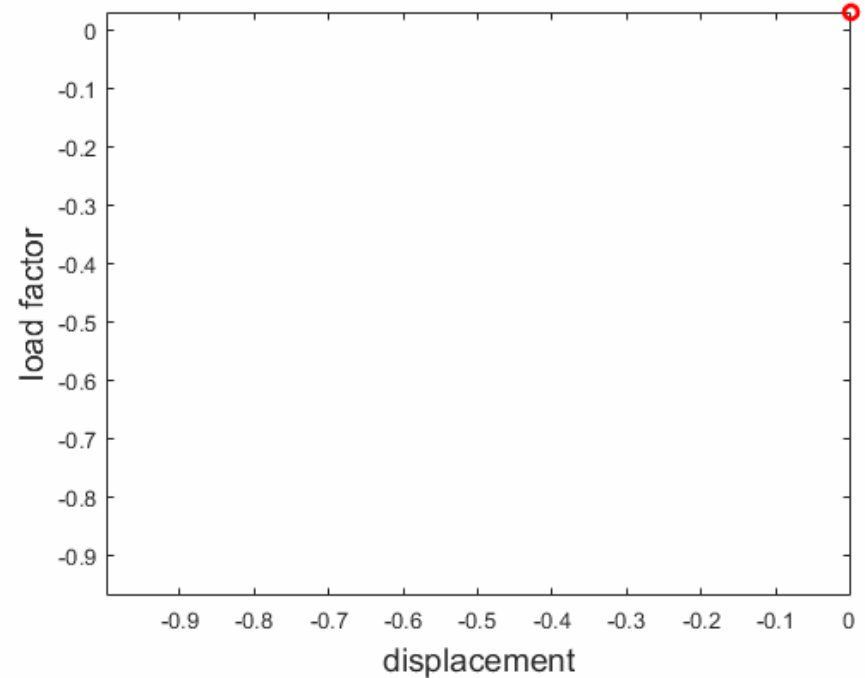
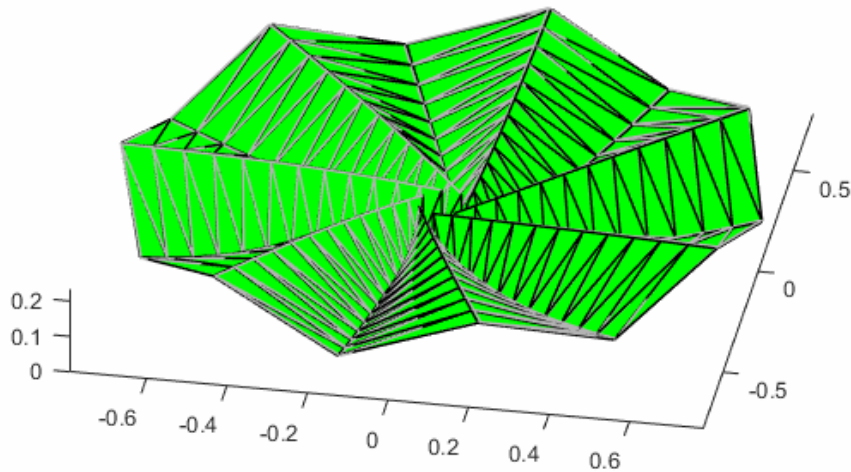


K. Liu and G. H. Paulino, "Nonlinear mechanics of non-rigid origami: an efficient computational approach," *Proceedings of the Royal Society A: Mathematical, Physical and Engineering Sciences*, vol. 473, 2017.

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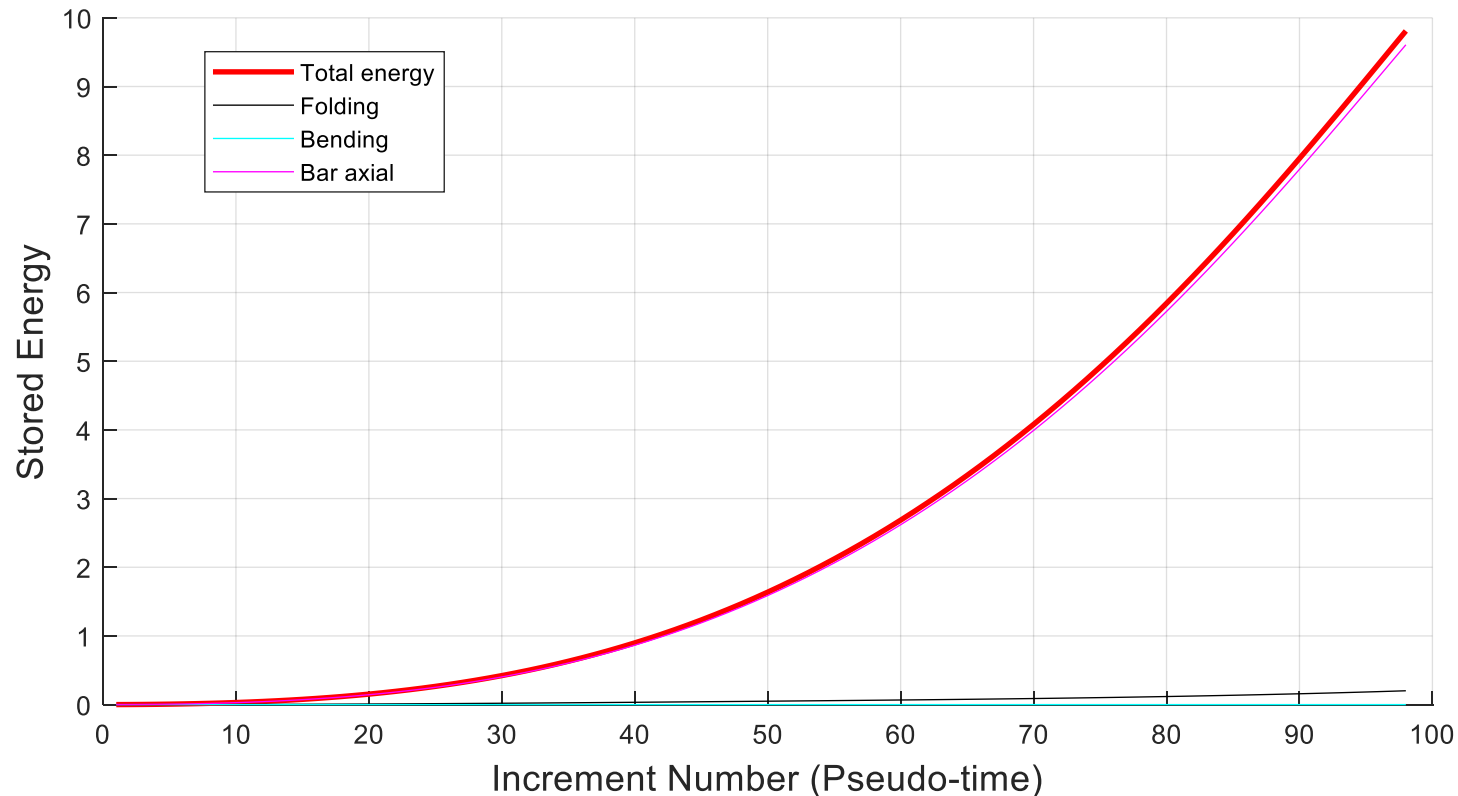
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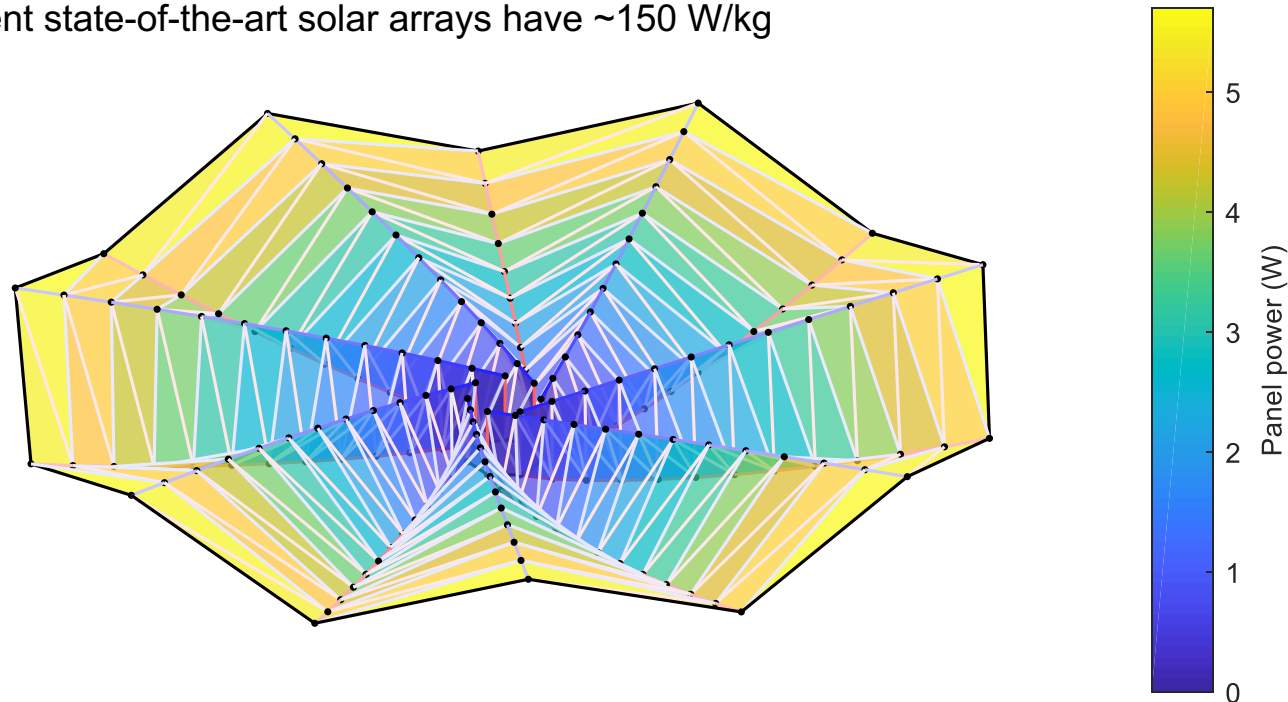


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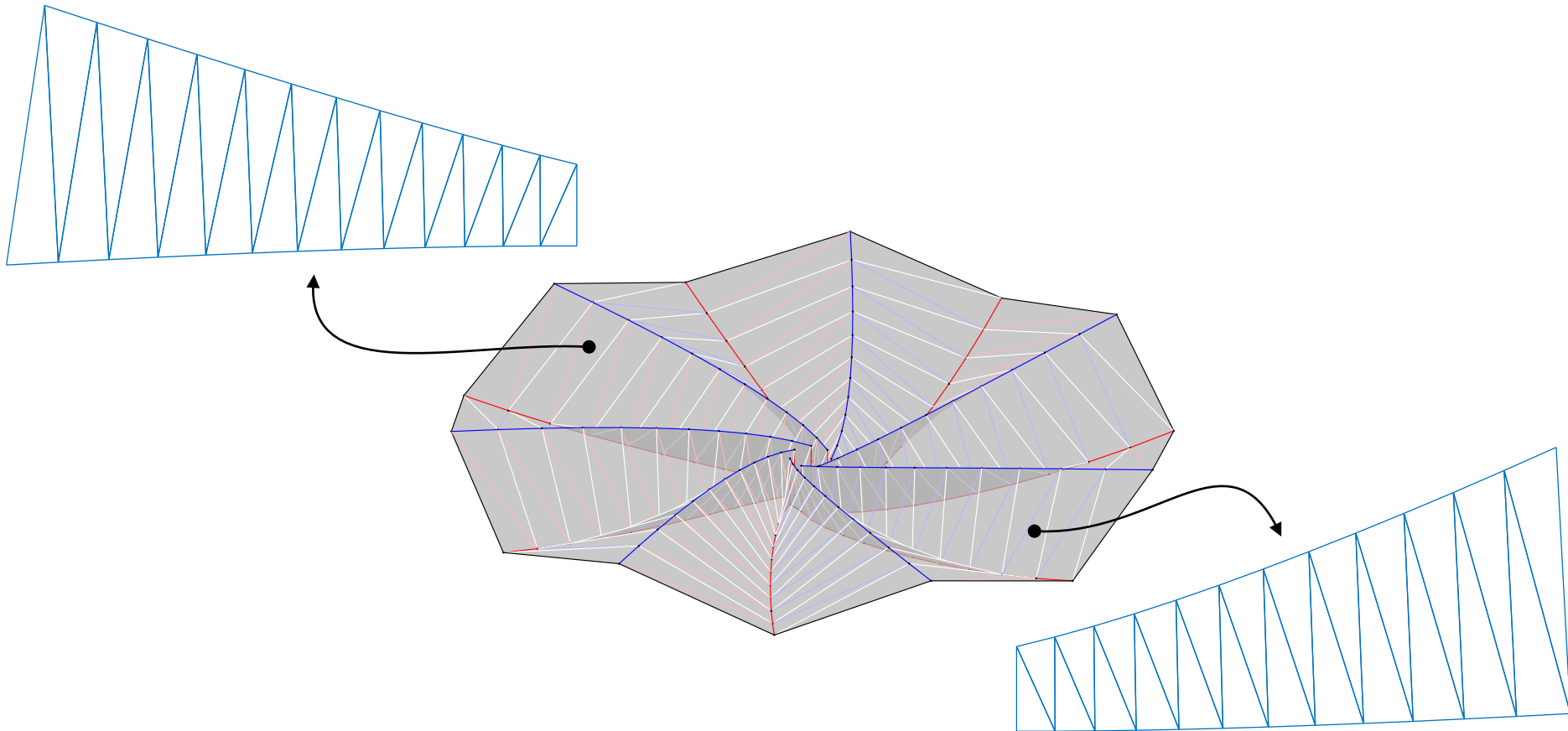
# Solar array performance

- Using an example array ( $N = 7$ , unfolded diameter = 1.584m)
  - Collected power (at normal solar incidence) = 835 W
  - Power for an equivalent flat plate = 875 W
  - Corrugated surface collects 95% of the power from an equivalent flat plate
- Loss mechanisms for panels due to local angle-of-incidence effects
  - Geometric loss ( $\cos(\theta)$ )
  - Reflective loss
- Can achieve specific power  $\sim 200$  W/kg
  - Current state-of-the-art solar arrays have  $\sim 150$  W/kg



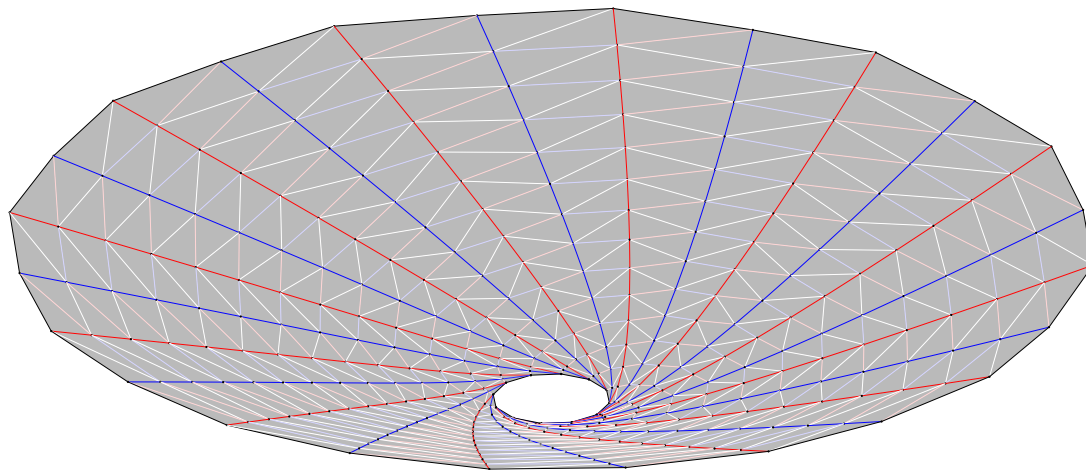
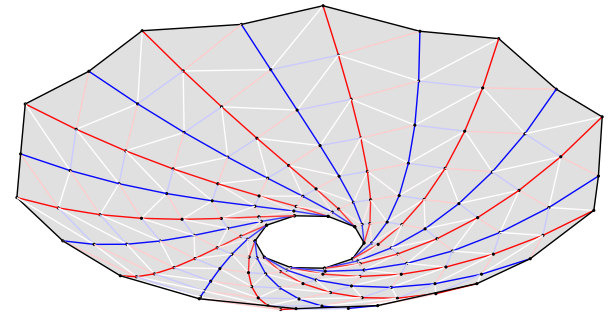
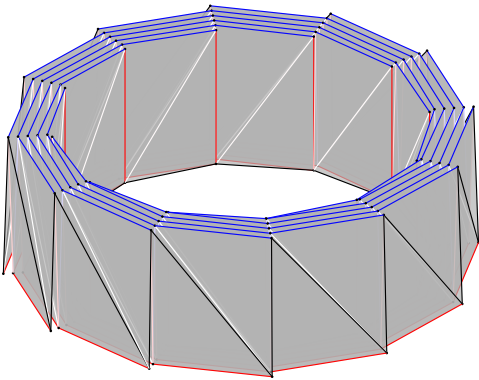
# Fabrication of physical models

- Each gore is a chain of triangles
  - Can fabricate each gore out of planar materials



# Extensions

- Can achieve different folded forms
- Can apply different objective functions to obtain different unfolded forms
  - e.g. cones, parabolas, and any other surface of revolution



# Conclusions

- Developed a novel origami wrapping pattern
  - Non-planar deployed forms for out-of-plane stiffness
  - Global thickness accommodation through designed spiral folded forms
- Flexible and powerful algorithm to generate target folded forms, or target unfolded forms
- Can be simply fabricated using planar materials
- Applicable to novel lightweight deployable solar array (200 W/kg, or 30% improvement over state-of-the-art)

# Acknowledgments

- Dr. Jonathan Grandidier assisted with the calculation of solar array power output.
- A part of this research was funded through the internal Research and Technology Development program at JPL. This research was carried out at the Jet Propulsion Laboratory, California Institute of Technology, under a contract with the National Aeronautics and Space Administration.

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